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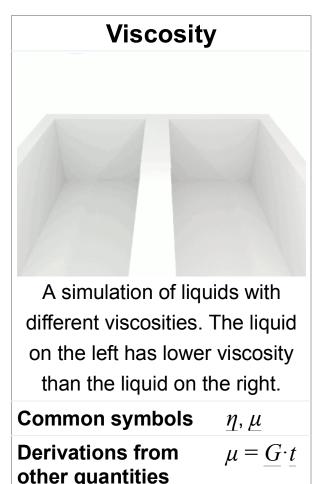
Viscosity

The **viscosity** of a <u>fluid</u> is a measure of its <u>resistance</u> to deformation at a given rate. For liquids, it corresponds to the informal concept of "thickness": for example, <u>syrup</u> has a higher viscosity than <u>water.^[1]</u>

Viscosity quantifies the internal <u>frictional force</u> between adjacent layers of fluid that are in relative motion. For instance, when a viscous fluid is forced through a tube, it flows more quickly near the tube's axis than near its walls. Experiments show that some <u>stress</u> (such as a <u>pressure</u> difference between the two ends of the tube) is needed to sustain the flow. This is because a force is required to overcome the friction between the layers of the fluid which are in relative motion. For a tube with a constant rate of flow, the strength of the compensating force is proportional to the fluid's viscosity.

In general, viscosity depends on a fluid's state, such as its temperature, pressure, and rate of deformation. However, the dependence on some of these properties is negligible in certain cases. For example, the viscosity of a <u>Newtonian fluid</u> does not vary significantly with the rate of deformation. Zero viscosity (no resistance to <u>shear stress</u>) is observed only at <u>very low temperatures</u> in <u>superfluids</u>; otherwise, the <u>second law of thermodynamics</u> requires all fluids to have positive viscosity.^{[2][3]} A fluid that has zero viscosity is called *ideal* or *inviscid*.

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Etymology

The word "viscosity" is derived from the Latin viscum ("mistletoe"). Viscum also referred to a viscous glue derived from mistletoe berries.^[4]

Definition

Dynamic viscosity

In <u>materials science</u> and <u>engineering</u>, one is often interested in understanding the forces or <u>stresses</u> involved in the <u>deformation</u> of a material. For instance, if the material were a simple spring, the answer would be given by <u>Hooke's law</u>, which says that the force experienced by a spring is proportional to the distance displaced from equilibrium. Stresses which can be attributed to the deformation of a material from some rest state are called <u>elastic</u> stresses. In other materials, stresses are present which can be attributed to the rate of

change of the deformation over time. These are called viscous stresses. For instance, in a fluid such as water the stresses which arise from shearing the fluid do not depend on the *distance* the fluid has been sheared; rather, they depend on how *quickly* the shearing occurs.

Viscosity is the material property which relates the viscous stresses in a material to the rate of change of a deformation (the strain rate). Although it applies to general flows, it is easy to visualize and define in a simple shearing flow, such as a planar <u>Couette flow</u>.

In the Couette flow, a fluid is trapped between two infinitely large plates, one fixed and one in parallel motion at constant speed **u** (see illustration to the right). If the speed of the top plate is low enough (to avoid turbulence), then in steady state the fluid particles move parallel to it, and their speed varies from **0** at the bottom to u at the top.^[5] Each layer of fluid moves faster than the one just below it, and friction between them gives rise to a force resisting their relative motion. In particular, the fluid applies on the top plate a force in the direction opposite to its motion, and an equal but opposite force on the bottom plate. An external force is therefore required in order to keep the top plate moving at constant speed.

In many fluids, the flow velocity is observed to vary linearly from zero at the bottom to **u** at the top. Moreover, the magnitude of the force, *F*, acting on the top plate is found to be proportional to the speed **u** and the area **A** of each plate, and inversely proportional to their separation **y**:

$$F=\mu Arac{u}{y}.$$

The proportionality factor is the *dynamic viscosity* of the fluid, often simply referred to as the *viscosity*. It is denoted by the Greek letter mu (μ). The dynamic viscosity has the dimensions (mass/length)/time, therefore resulting in the SI units and the derived units:

$$[\mu] = \frac{\text{kg}}{\text{m} \cdot \text{s}} = \frac{\text{N}}{\text{m}^2} \cdot \text{s} = \text{Pa} \cdot \text{s} = \text{pressure}$$
 multiplied by time.

The aforementioned ratio u/y is called the *rate of shear deformation* or *shear velocity*, and is the derivative of the fluid speed in the direction perpendicular to the normal vector of the plates (see illustrations to the right). If the velocity does not vary linearly with y, then the appropriate generalization is:

$$au=\murac{\partial u}{\partial y},$$

where $\tau = F/A$, and $\partial u/\partial y$ is the local shear velocity. This expression is referred to as Newton's law of viscosity. In shearing flows with planar symmetry, it is what defines μ . It is a special case of the general definition of viscosity (see below), which can be expressed in coordinate-free form.

Use of the Greek letter mu (μ) for the dynamic viscosity (sometimes also called the *absolute viscosity*) is common among mechanical and chemical engineers, as well as mathematicians and physicists. $\frac{[6][7][8]}{[6][7][8]}$ However, the Greek letter eta (η) is also used by chemists, physicists, and the IUPAC.^[9] The viscosity μ is sometimes also called the *shear viscosity*. However, at least one author discourages the use of this terminology, noting that μ can appear in non-shearing flows in addition to shearing flows.^[10]

Kinematic viscosity

In fluid dynamics, it is sometimes more appropriate to work in terms of kinematic viscosity (sometimes also called the momentum *diffusivity*), defined as the ratio of the dynamic viscosity (μ) over the density of the fluid (ρ). It is usually denoted by the Greek letter nu (*v*):

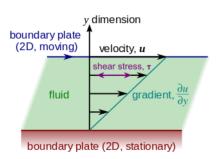
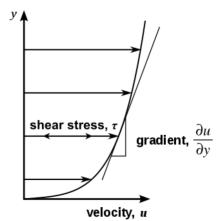


Illustration of a planar Couette flow. Since the shearing flow is opposed by friction between adjacent layers of fluid (which are in relative motion), a force is required to sustain the motion of the upper plate. The relative strength of this force is a measure of the fluid's viscosity.



In a general parallel flow, the shear stress is proportional to the gradient of the velocity.

 $u = -\frac{1}{\rho}$

and has the dimensions $(length)^2/time$, therefore resulting in the SI units and the derived units:

$$[\nu] = \frac{m^2}{s} = \frac{N \cdot m}{kg} \cdot s = \frac{J}{kg} \cdot s = \frac{specific \text{ energy multiplied by } time.}{$$

General definition

In very general terms, the viscous stresses in a fluid are defined as those resulting from the relative velocity of different fluid particles. As such, the viscous stresses must depend on spatial gradients of the flow velocity. If the velocity gradients are small, then to a first approximation the viscous stresses depend only on the first derivatives of the velocity.^[11] (For Newtonian fluids, this is also a linear dependence.) In Cartesian coordinates, the general relationship can then be written as

$$au_{ij} = \sum_k \sum_\ell \mu_{ijk\ell} rac{\partial v_k}{\partial r_\ell},$$

where $\mu_{ijk\ell}$ is a viscosity tensor that maps the <u>velocity gradient</u> tensor $\partial v_k / \partial r_\ell$ onto the viscous stress tensor τ_{ij} .^[12] Since the indices in this expression can vary from 1 to 3, there are 81 "viscosity coefficients" μ_{ijkl} in total. However, assuming that the viscosity rank-4 tensor is isotropic reduces these 81 coefficients to three independent parameters α , β , γ :

$$\mu_{ijk\ell} = lpha \delta_{ij} \delta_{k\ell} + eta \delta_{ik} \delta_{j\ell} + \gamma \delta_{i\ell} \delta_{jk},$$

and furthermore, it is assumed that no viscous forces may arise when the fluid is undergoing simple rigid-body rotation, thus $\beta = \gamma$, leaving only two independent parameters.^[11] The most usual decomposition is in terms of the standard (scalar) viscosity μ and the <u>bulk</u> viscosity κ such that $\alpha = \kappa - \frac{2}{3}\mu$ and $\beta = \gamma = \mu$. In vector notation this appears as:

$$oldsymbol{ au} = \mu \left[
abla \mathbf{v} + (
abla \mathbf{v})^\dagger
ight] - \left(rac{2}{3} \mu - \kappa
ight) (
abla \cdot \mathbf{v}) \delta,$$

where δ is the unit tensor, and the dagger \dagger denotes the <u>transpose</u>.^{[10][13]} This equation can be thought of as a generalized form of Newton's law of viscosity.

The bulk viscosity (also called volume viscosity) expresses a type of internal friction that resists the shearless compression or expansion of a fluid. Knowledge of κ is frequently not necessary in fluid dynamics problems. For example, an incompressible fluid satisfies $\nabla \cdot \mathbf{v} = \mathbf{0}$ and so the term containing κ drops out. Moreover, κ is often assumed to be negligible for gases since it is $\mathbf{0}$ in a monatomic ideal gas.^[10] One situation in which κ can be important is the calculation of energy loss in sound and shock waves, described by Stokes' law of sound attenuation, since these phenomena involve rapid expansions and compressions.

The defining equations for viscosity are not fundamental laws of nature, so their usefulness, as well as methods for measuring or calculating the viscosity, must be established using separate means. A potential issue is that viscosity depends, in principle, on the full microscopic state of the fluid, which encompasses the positions and momenta of every particle in the system.^[14] Such highly detailed information is typically not available in realistic systems. However, under certain conditions most of this information can be shown to be negligible. In particular, for Newtonian fluids near equilibrium and far from boundaries (bulk state), the viscosity depends only space- and time-dependent macroscopic fields (such as temperature and density) defining local equilibrium.^{[14][15]}

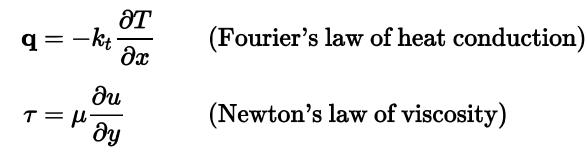
Nevertheless, viscosity may still carry a non-negligible dependence on several system properties, such as temperature, pressure, and the amplitude and frequency of any external forcing. Therefore, precision measurements of viscosity are only defined with respect to a specific fluid state.^[16] To standardize comparisons among experiments and theoretical models, viscosity data is sometimes extrapolated to ideal limiting cases, such as the *zero shear* limit, or (for gases) the *zero density* limit.

Momentum transport

Transport theory provides an alternative interpretation of viscosity in terms of momentum transport: viscosity is the material property which characterizes momentum transport within a fluid, just as thermal conductivity characterizes heat transport, and (mass) diffusivity characterizes mass transport.^[17] This perspective is implicit in Newton's law of viscosity, $\tau = \mu(\partial u/\partial y)$, because the shear stress τ has units equivalent to a momentum flux, i.e., momentum per unit time per unit area. Thus, τ can be interpreted as specifying the flow of momentum in the y direction from one fluid layer to the next. Per Newton's law of viscosity, this momentum flow occurs across a velocity gradient, and the magnitude of the corresponding momentum flux is determined by the viscosity.

The analogy with heat and mass transfer can be made explicit. Just as heat flows from high temperature to low temperature and mass flows from high density to low density, momentum flows from high velocity to low velocity. These behaviors are all described by compact expressions, called <u>constitutive relations</u>, whose one-dimensional forms are given here:

$$\mathbf{J}=-Drac{\partial
ho}{\partial x} \qquad ext{(Fick's law of diffusion)}$$



where ρ is the density, **J** and **q** are the mass and heat fluxes, and **D** and k_t are the mass diffusivity and thermal conductivity.^[18] The fact that mass, momentum, and energy (heat) transport are among the most relevant processes in continuum mechanics is not a coincidence: these are among the few physical quantities that are conserved at the microscopic level in interparticle collisions. Thus, rather than being dictated by the fast and complex microscopic interaction timescale, their dynamics occurs on macroscopic timescales, as described by the various equations of transport theory and hydrodynamics.

Newtonian and non-Newtonian fluids

Newton's law of viscosity is not a fundamental law of nature, but rather a constitutive equation (like Hooke's law, Fick's law, and Ohm's law) which serves to define the viscosity μ . Its form is motivated by experiments which show that for a wide range of fluids, μ is

independent of strain rate. Such fluids are called <u>Newtonian</u>. <u>Gases</u>, <u>water</u>, and many common liquids can be considered Newtonian in ordinary conditions and contexts. However, there are many <u>non-Newtonian</u> fluids that significantly deviate from this behavior. For example:

- <u>Shear-thickening</u> (dilatant) liquids, whose viscosity increases with the rate of shear strain.
- Shear-thinning liquids, whose viscosity decreases with the rate of shear strain.
- <u>Thixotropic</u> liquids, that become less viscous over time when shaken, agitated, or otherwise stressed.
- <u>Rheopectic</u> liquids, that become more viscous over time when shaken, agitated, or otherwise stressed.
- <u>Bingham plastics</u> that behave as a solid at low stresses but flow as a viscous fluid at high stresses.

<u>Trouton</u>'s ratio is the ratio of <u>extensional viscosity</u> to <u>shear viscosity</u>. For a Newtonian fluid, the Trouton ratio is 3.^{[19][20]} Shear-thinning liquids are very commonly, but misleadingly, described as thixotropic.^[21]

Even for a Newtonian fluid, the viscosity usually depends on its composition and temperature.

For gases and other <u>compressible fluids</u>, it depends on temperature and varies very slowly with pressure. The viscosity of some fluids may depend on other factors. A <u>magnetorheological fluid</u>, for example, becomes thicker when subjected to a <u>magnetic field</u>, possibly to the point of behaving like a solid.

In solids

The viscous forces that arise during fluid flow are distinct from the <u>elastic</u> forces that occur in a solid in response to shear, compression, or extension stresses. While in the latter the stress is proportional to the *amount* of shear deformation, in a fluid it is proportional to the *rate* of deformation over time. For this reason, <u>Maxwell</u> used the term *fugitive elasticity* for fluid viscosity.

However, many liquids (including water) will briefly react like elastic solids when subjected to sudden stress. Conversely, many "solids" (even granite) will flow like liquids, albeit very slowly, even under arbitrarily small stress.^[22] Such materials are best described as <u>viscoelastic</u>—that is, possessing both elasticity (reaction to deformation) and viscosity (reaction to rate of deformation).

Viscoelastic solids may exhibit both shear viscosity and bulk viscosity. The <u>extensional viscosity</u> is a <u>linear combination</u> of the shear and bulk viscosities that describes the reaction of a solid elastic material to elongation. It is widely used for characterizing polymers.

In geology, earth materials that exhibit viscous deformation at least three <u>orders of magnitude</u> greater than their elastic deformation are sometimes called rheids.^[23]

Measurement

Viscosity is measured with various types of <u>viscometers</u> and <u>rheometers</u>. A rheometer is used for fluids that cannot be defined by a single value of viscosity and therefore require more parameters to be set and measured than is the case for a viscometer. Close temperature control of the fluid is essential to obtain accurate measurements, particularly in materials like lubricants, whose viscosity can double with a change of only 5 $^{\circ}C.$ ^[24]

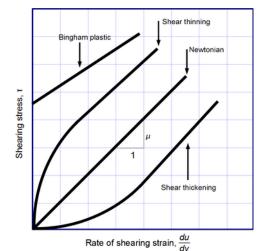
For some fluids, the viscosity is constant over a wide range of shear rates (<u>Newtonian fluids</u>). The fluids without a constant viscosity (<u>non-Newtonian fluids</u>) cannot be described by a single number. Non-Newtonian fluids exhibit a variety of different correlations between shear stress and shear rate.

One of the most common instruments for measuring kinematic viscosity is the glass capillary viscometer.

In <u>coating</u> industries, viscosity may be measured with a cup in which the <u>efflux time</u> is measured. There are several sorts of cup—such as the <u>Zahn cup</u> and the <u>Ford viscosity cup</u>—with the usage of each type varying mainly according to the industry.

Also used in coatings, a *Stormer viscometer* employs load-based rotation to determine viscosity. The viscosity is reported in Krebs units (KU), which are unique to Stormer viscometers.

Vibrating viscometers can also be used to measure viscosity. Resonant, or vibrational viscometers work by creating shear waves within the liquid. In this method, the sensor is submerged in the fluid and is made to resonate at a specific frequency. As the surface of the sensor shears through the liquid, energy is lost due to its viscosity. This dissipated energy is then measured and converted into a viscosity reading. A higher viscosity causes a greater loss of energy.



Viscosity, the slope of each line, varies among materials.

Extensional viscosity can be measured with various rheometers that apply extensional stress.

Volume viscosity can be measured with an acoustic rheometer.

<u>Apparent viscosity</u> is a calculation derived from tests performed on <u>drilling fluid</u> used in oil or gas well development. These calculations and tests help engineers develop and maintain the properties of the drilling fluid to the specifications required.

Nanoviscosity (viscosity sensed by nanoprobes) can be measured by fluorescence correlation spectroscopy.^[25]

Units

The <u>SI</u> unit of dynamic viscosity is the <u>newton</u>-second per square meter (N·s/m²), also frequently expressed in the equivalent forms <u>pascal-second</u> (Pa·s), <u>kilogram</u> per meter per second (kg·m⁻¹·s⁻¹) and <u>Poiseuilli</u> (Pl). The <u>CGS</u> unit is the <u>poise</u> (P, or g·cm⁻¹·s⁻¹ = 0.1 Pa·s), <u>[26]</u> named after <u>Jean Léonard Marie Poiseuille</u>. It is commonly expressed, particularly in <u>ASTM</u> standards, as *centipoise* (cP). The centipoise is convenient because the viscosity of water at 20 °C is about 1 cP, and one centipoise is equal to the SI millipascal second (mPa·s).

The SI unit of kinematic viscosity is square meter per second (m²/s), whereas the CGS unit for kinematic viscosity is the **stokes** (St, or $cm^2 \cdot s^{-1} = 0.0001 \ m^2 \cdot s^{-1}$), named after Sir <u>George Gabriel Stokes</u>. [27] In U.S. usage, *stoke* is sometimes used as the singular form. The <u>submultiple centistokes</u> (cSt) is often used instead, 1 cSt = 1 mm² \cdot s^{-1} = 10⁻⁶ m² \cdot s^{-1}. The kinematic viscosity of water at 20 °C is about 1

cSt.

The most frequently used systems of <u>US customary</u>, or Imperial, units are the <u>British Gravitational</u> (BG) and <u>English Engineering</u> (EE). In the BG system, dynamic viscosity has units of <u>pound</u>-seconds per square foot ($lb\cdot s/ft^2$), and in the EE system it has units of <u>pound-force</u>-seconds per square foot ($lbf\cdot s/ft^2$). The pound and pound-force are equivalent; the two systems differ only in how force and mass are defined. In the BG system the pound is a basic unit from which the unit of mass (the <u>slug</u>) is defined by <u>Newton's Second Law</u>, whereas in the EE system the units of force and mass (the pound-force and <u>pound-mass</u> respectively) are defined independently through the Second Law using the proportionality constant g_c .

Kinematic viscosity has units of square feet per second (ft²/s) in both the BG and EE systems.

Nonstandard units include the <u>reyn</u>, a British unit of dynamic viscosity. In the automotive industry the <u>viscosity index</u> is used to describe the change of viscosity with temperature.

The <u>reciprocal</u> of viscosity is *fluidity*, usually symbolized by $\phi = 1/\mu$ or $F = 1/\mu$, depending on the convention used, measured in *reciprocal poise* (P⁻¹, or cm·s·g⁻¹), sometimes called the *rhe*. Fluidity is seldom used in engineering practice.

At one time the petroleum industry relied on measuring kinematic viscosity by means of the <u>Saybolt viscometer</u>, and expressing kinematic viscosity in units of <u>Saybolt universal seconds</u> (SUS).^[28] Other abbreviations such as SSU (*Saybolt seconds universal*) or SUV (*Saybolt universal viscosity*) are sometimes used. Kinematic viscosity in centistokes can be converted from SUS according to the arithmetic and the reference table provided in <u>ASTM</u> D 2161.

Molecular origins

Momentum transport in gases is mediated by discrete molecular collisions, and in liquids by attractive forces that bind molecules close together.^[17] Because of this, the dynamic viscosities of liquids are typically much larger than those of gases. In addition, viscosity tends to increase with temperature in gases and decrease with temperature in liquids.

Above the liquid-gas <u>critical point</u>, the liquid and gas phases are replaced by a single <u>supercritical phase</u>. In this regime, the mechanisms of momentum transport interpolate between liquid-like and gas-like behavior. For example, along a supercritical <u>isobar</u> (constant-pressure surface), the kinematic viscosity decreases at low temperature and increases at high temperature, with a minimum in between. [29][30] A rough estimate for the value at the minimum is

$$u_{
m min} = rac{1}{4\pi} rac{\hbar}{\sqrt{m_e m}}$$

where \hbar is <u>Planck's constant</u>, m_e is the <u>electron mass</u>, and m is the molecular mass.^[30]

In general, however, the viscosity of a system depends in detail on how the molecules constituting the system interact, and there are no simple but correct formulas for it. The simplest exact expressions are the <u>Green–Kubo relations</u> for the linear shear viscosity or the *transient time correlation function* expressions derived by Evans and Morriss in 1988.^[31] Although these expressions are each exact, calculating the viscosity of a dense fluid using these relations currently requires the use of <u>molecular dynamics</u> computer simulations. Somewhat more progress can be made for a dilute gas, as elementary assumptions about how gas molecules move and interact lead to a basic understanding of the molecular origins of viscosity. More sophisticated treatments can be constructed by systematically coarse-graining the <u>equations of motion</u> of the gas molecules. An example of such a treatment is <u>Chapman–Enskog theory</u>, which derives expressions for the viscosity of a dilute gas from the Boltzmann equation.^[15]

Pure gases

Elementary calculation of viscosity for a dilute gas

Consider a dilute gas moving parallel to the x-axis with velocity u(y) that depends only on the y coordinate. To simplify the discussion, the gas is assumed to have uniform temperature and density.

Under these assumptions, the $m{x}$ velocity of a molecule passing through $m{y}=0$

is equal to whatever velocity that molecule had when its mean free path λ began. Because λ is typically small compared with macroscopic scales, the average *x* velocity of such a molecule has the form

$$u(0)\pm lpha\lambdarac{du}{dy}(0),$$

where α is a numerical constant on the order of 1. (Some authors estimate $\alpha = 2/3$;^{[17][32]} on the other hand, a more careful calculation for rigid elastic spheres gives $\alpha \simeq 0.998$.) Next, because half the molecules on either side are moving towards y = 0, and doing so on average with half the <u>average</u> molecular speed $(8k_{\rm B}T/\pi m)^{1/2}$, the momentum flux from either side is

$$rac{1}{4}
ho\cdot\sqrt{rac{8k_{
m B}T}{\pi m}}\cdot\left(u(0)\pmlpha\lambdarac{du}{dy}(0)
ight).$$

The net momentum flux at y = 0 is the difference of the two:

$$-rac{1}{2}
ho\cdot\sqrt{rac{8k_{
m B}T}{\pi m}}\cdotlpha\lambdarac{du}{dy}(0).$$

According to the definition of viscosity, this momentum flux should be equal to

$$-\mu rac{du}{dy}(0)$$
, which leads to $\mu = lpha
ho \lambda \sqrt{rac{2k_{
m B}T}{\pi m_{
m c}}}$

Viscosity in gases arises principally from the molecular diffusion that transports momentum between layers of flow. An elementary calculation for a dilute gas at temperature
$$T$$
 and density ρ gives

$$\mu = lpha
ho \lambda \sqrt{rac{2k_{
m B}T}{\pi m}},$$

where $k_{\rm B}$ is the <u>Boltzmann constant</u>, *m* the molecular mass, and α a numerical constant on the order of **1**. The quantity λ , the <u>mean free</u> <u>path</u>, measures the average distance a molecule travels between collisions. Even without *a priori* knowledge of α , this expression has nontrivial implications. In particular, since λ is typically inversely proportional to density and increases with temperature, μ itself should increase with temperature and be independent of density at fixed temperature. In fact, both of these predictions persist in more sophisticated treatments, and accurately describe experimental observations. By contrast, liquid viscosity typically decreases with temperature. [17][32]

For rigid elastic spheres of diameter σ , λ can be computed, giving

$$\mu = rac{lpha}{\pi^{3/2}} rac{\sqrt{k_{
m B}mT}}{\sigma^2}$$

In this case λ is independent of temperature, so $\mu \propto T^{1/2}$. For more complicated molecular models, however, λ depends on temperature in a non-trivial way, and simple kinetic arguments as used here are inadequate. More fundamentally, the notion of a mean free path becomes imprecise for particles that interact over a finite range, which limits the usefulness of the concept for describing real-world gases.^[33]

Chapman–Enskog theory

A technique developed by <u>Sydney Chapman</u> and <u>David Enskog</u> in the early 1900s allows a more refined calculation of μ .^[15] It is based on the <u>Boltzmann equation</u>, which provides a statistical description of a dilute gas in terms of intermolecular interactions.^[34] The technique allows accurate calculation of μ for molecular models that are more realistic than rigid elastic spheres, such as those incorporating intermolecular attractions. Doing so is necessary to reproduce the correct temperature dependence of μ , which experiments show increases more rapidly than the $T^{1/2}$ trend predicted for rigid elastic spheres.^[17] Indeed, the Chapman–Enskog analysis shows that the predicted temperature dependence can be tuned by varying the parameters in various molecular models. A simple example is the Sutherland model,^[a] which describes rigid elastic spheres with *weak* mutual attraction. In such a case, the attractive force can be treated perturbatively, which leads to a simple expression for μ :

$$\mu = rac{5}{16 \sigma^2} igg(rac{k_{
m B} m T}{\pi} igg)^{1/2} igg(1 + rac{S}{T} igg)^{-1},$$

where S is independent of temperature, being determined only by the parameters of the intermolecular attraction. To connect with experiment, it is convenient to rewrite as

$$\mu=\mu_0\left(rac{T}{T_0}
ight)^{3/2}rac{T_0+S}{T+S},$$

where μ_0 is the viscosity at temperature T_0 .^[35] If μ is known from experiments at $T = T_0$ and at least one other temperature, then S can be calculated. Expressions for μ obtained in this way are qualitatively accurate for a number of simple gases. Slightly more sophisticated models, such as the Lennard-Jones potential, may provide better agreement with experiments, but only at the cost of a more opaque dependence on temperature. In some systems, the assumption of spherical symmetry must be abandoned as well, as is the case for vapors with highly polar molecules like H₂O. In these cases, the Chapman–Enskog analysis is significantly more complicated.^{[36][37]}

Bulk viscosity

In the kinetic-molecular picture, a non-zero bulk viscosity arises in gases whenever there are non-negligible relaxational timescales governing the exchange of energy between the translational energy of molecules and their internal energy, e.g. rotational and vibrational. As such, the bulk viscosity is **0** for a monatomic ideal gas, in which the internal energy of molecules in negligible, but is nonzero for a gas like <u>carbon dioxide</u>, whose molecules possess both rotational and vibrational energy.^{[38][39]}

Pure liquids

In contrast with gases, there is no simple yet accurate picture for the molecular origins of viscosity in liquids.

At the simplest level of description, the relative motion of adjacent layers in a liquid is opposed primarily by attractive molecular forces acting across the layer boundary. In this picture, one (correctly) expects viscosity to decrease with increasing temperature. This is because increasing temperature increases the random thermal motion of the molecules, which makes it easier for them to overcome their attractive interactions.^[40]

Building on this visualization, a simple theory can be constructed in analogy with the discrete structure of a solid: groups of molecules in a liquid are visualized as forming "cages" which surround and enclose single molecules.^[41] These cages can be occupied or unoccupied, and stronger molecular attraction corresponds to stronger cages. Due to random thermal motion, a molecule "hops" between cages at a rate which varies inversely with the strength of molecular attractions. In <u>equilibrium</u> these "hops" are not biased in any direction. On the other hand, in order for two adjacent layers to move relative to each other, the "hops" must be biased in the direction of the relative motion. The force required to sustain this directed motion can be estimated for a given shear rate, leading to



0:15

Video showing three liquids with different viscosities



Experiment showing the behavior of a viscous fluid with blue dye for visibility

(1)

 $\mu pprox rac{N_A h}{V} \expigg(3.8 rac{T_b}{T} igg),$

where N_A is the <u>Avogadro constant</u>, h is the <u>Planck constant</u>, V is the volume of a <u>mole</u> of liquid, and T_b is the <u>normal boiling point</u>. This result has the same form as the well-known empirical relation

$$\mu = A e^{B/T}, \tag{2}$$

where A and B are constants fit from data.^{[41][42]} On the other hand, several authors express caution with respect to this model. Errors as large as 30% can be encountered using equation (1), compared with fitting equation (2) to experimental data.^[41] More fundamentally, the physical assumptions underlying equation (1) have been criticized.^[43] It has also been argued that the exponential dependence in equation (1) does not necessarily describe experimental observations more accurately than simpler, non-exponential expressions.^{[44][45]}

In light of these shortcomings, the development of a less ad hoc model is a matter of practical interest. Foregoing simplicity in favor of precision, it is possible to write rigorous expressions for viscosity starting from the fundamental equations of motion for molecules. A classic example of this approach is Irving–Kirkwood theory.^[46] On the other hand, such expressions are given as averages over multiparticle <u>correlation functions</u> and are therefore difficult to apply in practice.

In general, empirically derived expressions (based on existing viscosity measurements) appear to be the only consistently reliable means of calculating viscosity in liquids. [47]

Mixtures and blends

Gaseous mixtures

The same molecular-kinetic picture of a single component gas can also be applied to a gaseous mixture. For instance, in the Chapman-Enskog approach the viscosity μ_{mix} of a binary mixture of gases can be written in terms of the individual component viscosities $\mu_{1,2}$, their respective volume fractions, and the intermolecular interactions.^[15] As for the single-component gas, the dependence of μ_{mix} on the parameters of the intermolecular interactions enters through various collisional integrals which may not be expressible in terms of elementary functions. To obtain usable expressions for μ_{mix} which reasonably match experimental data, the collisional integrals typically must be evaluated using some combination of analytic calculation and empirical fitting. An example of such a procedure is the Sutherland approach for the single-component gas, discussed above.

Blends of liquids

As for pure liquids, the viscosity of a blend of liquids is difficult to predict from molecular principles. One method is to extend the molecular "cage" theory presented above for a pure liquid. This can be done with varying levels of sophistication. One expression resulting from such an analysis is the Lederer–Roegiers equation for a binary mixture:

$$\ln \mu_{ ext{blend}} = rac{x_1}{x_1+lpha x_2} \ln \mu_1 + rac{lpha x_2}{x_1+lpha x_2} \ln \mu_2,$$

where α is an empirical parameter, and $x_{1,2}$ and $\mu_{1,2}$ are the respective mole fractions and viscosities of the component liquids. [48]

Since blending is an important process in the lubricating and oil industries, a variety of empirical and propriety equations exist for predicting the viscosity of a blend.^[48]

Solutions and suspensions

Aqueous solutions

Depending on the <u>solute</u> and range of concentration, an aqueous <u>electrolyte</u> solution can have either a larger or smaller viscosity compared with pure water at the same temperature and pressure. For instance, a 20% saline (<u>sodium chloride</u>) solution has viscosity over 1.5 times that of pure water, whereas a 20% potassium iodide solution has viscosity about 0.91 times that of pure water.

An idealized model of dilute electrolytic solutions leads to the following prediction for the viscosity μ_s of a solution: [49]

$$rac{\mu_s}{\mu_0} = 1 + A \sqrt{c},$$

where μ_0 is the viscosity of the solvent, *c* is the concentration, and *A* is a positive constant which depends on both solvent and solute properties. However, this expression is only valid for very dilute solutions, having *c* less than 0.1 mol/L.^[50] For higher concentrations, additional terms are necessary which account for higher-order molecular correlations:

$$rac{\mu_s}{\mu_0} = 1 + A\sqrt{c} + Bc + Cc^2,$$

where B and C are fit from data. In particular, a negative value of B is able to account for the decrease in viscosity observed in some solutions. Estimated values of these constants are shown below for sodium chloride and potassium iodide at temperature 25 °C (mol = mole, L = liter).^[49]

Solute	A (mol ^{-1/2} L ^{1/2})	<i>B</i> (mol ^{−1} L)	C (mol ⁻² L ²)
Sodium chloride (NaCl)	0.0062	0.0793	0.0080
Potassium iodide (KI)	0.0047	-0.0755	0.0000

Suspensions

In a suspension of solid particles (e.g. micron-size spheres suspended in oil), an effective viscosity μ_{eff} can be defined in terms of stress and strain components which are averaged over a volume large compared with the distance between the suspended particles, but small with respect to macroscopic dimensions.^[51] Such suspensions generally exhibit non-Newtonian behavior. However, for dilute systems in steady flows, the behavior is Newtonian and expressions for μ_{eff} can be derived directly from the particle dynamics. In a very dilute system, with volume fraction $\phi \leq 0.02$, interactions between the suspended particles can be ignored. In such a case one can explicitly calculate the flow field around each particle independently, and combine the results to obtain μ_{eff} . For spheres, this results in the Einstein equation:

$$\mu_{ ext{eff}} = \mu_0 \left(1 + rac{5}{2} \phi
ight),$$

where μ_0 is the viscosity of the suspending liquid. The linear dependence on ϕ is a consequence of neglecting interparticle interactions. For dilute systems in general, one expects μ_{eff} to take the form

$$\mu_{ ext{eff}} = \mu_0 \left(1 + B \phi
ight),$$

where the coefficient B may depend on the particle shape (e.g. spheres, rods, disks).^[52] Experimental determination of the precise value of B is difficult, however: even the prediction B = 5/2 for spheres has not been conclusively validated, with various experiments finding values in the range $1.5 \leq B \leq 5$. This deficiency has been attributed to difficulty in controlling experimental conditions.^[53]

In denser suspensions, μ_{eff} acquires a nonlinear dependence on ϕ , which indicates the importance of interparticle interactions. Various analytical and semi-empirical schemes exist for capturing this regime. At the most basic level, a term quadratic in ϕ is added to μ_{eff} :

$$\mu_{ ext{eff}} = \mu_0 \left(1 + B \phi + B_1 \phi^2
ight),$$

and the coefficient B_1 is fit from experimental data or approximated from the microscopic theory. However, some authors advise caution in applying such simple formulas since non-Newtonian behavior appears in dense suspensions ($\phi \gtrsim 0.25$ for spheres),^[53] or in suspensions of elongated or flexible particles.^[51]

There is a distinction between a suspension of solid particles, described above, and an <u>emulsion</u>. The latter is a suspension of tiny droplets, which themselves may exhibit internal circulation. The presence of internal circulation can decrease the observed effective viscosity, and different theoretical or semi-empirical models must be used.^[54]

Amorphous materials

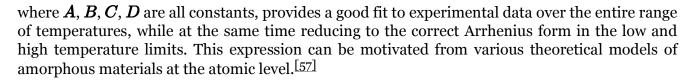
In the high and low temperature limits, viscous flow in <u>amorphous</u> materials (e.g. in glasses and melts)[56][57][58] has the Arrhenius form:

$$\mu = A e^{Q/(RT)},$$

where Q is a relevant <u>activation energy</u>, given in terms of molecular parameters; T is temperature; R is the molar <u>gas constant</u>; and A is approximately a constant. The activation energy Q takes a different value depending on whether the high or low temperature limit is being considered: it changes from a high value $Q_{\rm H}$ at low temperatures (in the glassy state) to a low value $Q_{\rm L}$ at high temperatures (in the liquid state).

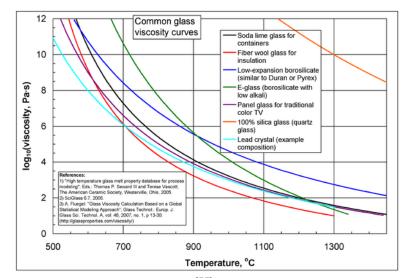
For intermediate temperatures, Q varies nontrivially with temperature and the simple Arrhenius form fails. On the other hand, the two-exponential equation

$$\mu = AT \exp\left(rac{B}{RT}
ight) \left[1+C \exp\left(rac{D}{RT}
ight)
ight],$$

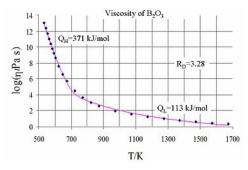


A two-exponential equation for the viscosity can be derived within the Dyre shoving model of supercooled liquids, where the Arrhenius energy barrier is identified with the high-frequency shear modulus times a characteristic shoving volume.^{[59][60]} Upon specifying the temperature dependence of the shear modulus via thermal expansion and via the repulsive part of the intermolecular potential, another two-exponential equation is retrieved:^[61]

$$\mu = \exp\left\{rac{V_c C_G}{k_B T}\exp\left[(2+\lambda)lpha_T T_g\left(1-rac{T}{T_g}
ight)
ight]
ight\}$$



Common glass viscosity curves^[55]



<u>Common logarithm</u> of viscosity against temperature for B_2O_3 , showing two regimes

where C_G denotes the high-frequency <u>shear modulus</u> of the material evaluated at a temperature equal to the <u>glass transition</u> temperature T_g , V_c is the so-called shoving volume, i.e. it is the characteristic volume of the group of atoms involved in the shoving event by which an atom/molecule escapes from the cage of nearest-neighbours, typically on the order of the volume occupied by few atoms. Furthermore, α_T is the <u>thermal expansion</u> coefficient of the material, λ is a parameter which measures the steepness of the power-law rise of the ascending flank of the first peak of the <u>radial distribution function</u>, and is quantitatively related to the repulsive part of the <u>interatomic potential</u>.^[61] Finally, k_B denotes the <u>Boltzmann constant</u>.

Eddy viscosity

In the study of <u>turbulence</u> in <u>fluids</u>, a common practical strategy is to ignore the small-scale <u>vortices</u> (or <u>eddies</u>) in the motion and to calculate a large-scale motion with an *effective* viscosity, called the "eddy viscosity", which characterizes the transport and dissipation of <u>energy</u> in the smaller-scale flow (see <u>large eddy simulation</u>).^{[62][63]} In contrast to the viscosity of the fluid itself, which must be positive by the second law of thermodynamics, the eddy viscosity can be negative.^{[64][65]}

Prediction

Because viscosity depends continuously on temperature and pressure, it cannot be fully characterized by a finite number of experimental measurements. Predictive formulas become necessary if experimental values are not available at the temperatures and pressures of interest. This capability is important for thermophysical simulations, in which the temperature and pressure of a fluid can vary continuously with space and time. A similar situation is encountered for mixtures of pure fluids, where the viscosity depends continuously on the concentration ratios of the constituent fluids

For the simplest fluids, such as dilute monatomic gases and their mixtures, <u>*ab initio* quantum mechanical</u> computations can accurately predict viscosity in terms of fundamental atomic constants, i.e., without reference to existing viscosity measurements. [66] For the special case of dilute helium, <u>uncertainties</u> in the <u>*ab initio*</u> calculated viscosity are two order of magnitudes smaller than uncertainties in experimental values. [67]

For most fluids, such high-accuracy, first-principles computations are not feasible. Rather, theoretical or empirical expressions must be fit to existing viscosity measurements. If such an expression is fit to high-fidelity data over a large range of temperatures and pressures, then it is called a "reference correlation" for that fluid. Reference correlations have been published for many pure fluids; a few examples are water, carbon dioxide, ammonia, benzene, and xenon.^{[68][69][70][71][72]} Many of these cover temperature and pressure ranges that encompass gas, liquid, and supercritical phases.

Thermophysical modeling software often relies on reference correlations for predicting viscosity at user-specified temperature and pressure. These correlations may be proprietary. Examples are <u>REFPROP^[73]</u> (proprietary) and <u>CoolProp^[74]</u> (open-source).

Viscosity can also be computed using formulas that express it in terms of the statistics of individual particle trajectories. These formulas include the <u>Green–Kubo relations</u> for the linear shear viscosity and the *transient time correlation function* expressions derived by Evans and Morriss in 1988.^{[75][31]} The advantage of these expressions is that they are formally exact and valid for general systems. The

disadvantage is that they require detailed knowledge of particle trajectories, available only in computationally expensive simulations such as <u>molecular dynamics</u>. An accurate model for interparticle interactions is also required, which may be difficult to obtain for complex molecules.^[76]

Selected substances

Observed values of viscosity vary over several orders of magnitude, even for common substances (see the order of magnitude table below). For instance, a 70% sucrose (sugar) solution has a viscosity over 400 times that of water, and 26000 times that of air.^[78] More dramatically, pitch has been estimated to have a viscosity 230 billion times that of water.^[77]

Water

The <u>dynamic viscosity</u> μ of <u>water</u> is about 0.89 mPa·s at room temperature (25 °C). As a function of temperature in <u>kelvins</u>, the viscosity can be estimated using the semi-empirical <u>Vogel-Fulcher-Tammann</u> equation:

$$\mu = A \exp \left(rac{B}{T-C}
ight)$$

where A = 0.02939 mPa·s, B = 507.88 K, and C = 149.3 K.^[79] Experimentally determined values of the viscosity are also given in the table below. The values at 20 °C are a useful reference: there, the dynamic viscosity is about 1 cP and the kinematic viscosity is about 1 cSt.

Viscosity of water at various temperatures^[78]

Temperature (°C)	Viscosity (mPa⋅s or cP)	
10	1.3059	
20	1.0016	
30	0.79722	
50	0.54652	
70	0.40355	
90	0.31417	

Air

Under standard atmospheric conditions (25 °C and pressure of 1 bar), the dynamic viscosity of air is 18.5 μ Pa·s, roughly 50 times smaller than the viscosity of water at the same temperature. Except at very high pressure, the viscosity of air depends mostly on the temperature. Among the many possible approximate formulas for the temperature dependence (see Temperature dependence of viscosity), one is:^[80]

$$\eta_{
m air} = 2.791 \cdot 10^{-7} \cdot T^{0.7355}$$

which is accurate in the range -20 °C to 400 °C. For this formula to be valid, the temperature must be given in <u>kelvins</u>; η_{air} then corresponds to the viscosity in Pa·s.

Other common substances

Substance	Viscosity (mPa⋅s)	Temperature (°C)	Ref.
Benzene	0.604	25	
Water	1.0016	20	[78]
Mercury	1.526	25	
Whole milk	2.12	20	[81]
Dark beer	2.53	20	
Olive oil	56.2	26	[81]
Honey	≈ 2000–10000	20	[82]
Ketchup ^[b]	≈ 5000–20000	25	[83]
Peanut butter ^[b]	$\approx 10^{4} - 10^{6}$		[84]
Pitch	2.3 × 10 ¹¹	10–30 (variable)	[77]



Queensland <u>pitch drop</u> <u>experiment</u>, pitch has been dripping slowly through a funnel since 1927, at a rate of one drop roughly every decade. In this way the viscosity of pitch has been determined to be approximately 230 billion (2.3×10^{11}) times that of water.[77]



Honey being drizzled

Order of magnitude estimates

The following table illustrates the range of viscosity values observed in common substances. Unless otherwise noted, a temperature of 25 °C and a pressure of 1 atmosphere are assumed.

The values listed are representative estimates only, as they do not account for measurement uncertainties, variability in material definitions, or non-Newtonian behavior.

Factor (Pa·s)	Description	Examples	Values (Pa·s)	Ref.
10 ⁻⁶	Lower range of gaseous viscosity	Butane	7.49 × 10 ⁻⁶	[85]
		Hydrogen	8.8 × 10 ⁻⁶	[86]
10 ⁻⁵	Upper range of gaseous viscosity	Krypton	2.538 × 10 ⁻⁵	[87]
		Neon	3.175 × 10 ⁻⁵	
10 ⁻⁴ Lower range of	Lower range of liquid viscosity	Pentane	2.24 × 10 ⁻⁴	[78]
		Gasoline	6 × 10 ⁻⁴	
		Water	8.90 × 10 ⁻⁴	
		Ethanol	1.074 × 10 ^{−3}	[78]
		Mercury	1.526 × 10 ⁻³	
	Typical range for small-molecule Newtonian liquids	Whole milk (20 °C)	2.12 × 10 ⁻³	[81]
		Blood	3×10^{-3} to 6×10^{-3}	[88]
		Liquid steel (1550 °C)	6 × 10 ⁻³	[89]
		Linseed oil	0.028	
		Oleic acid	0.036	[90]
		Olive oil	0.084	[81]
		SAE 10 Motor oil	0.085 to 0.14	
10 ⁻² – 10 ⁰	Oils and long-chain hydrocarbons	Castor oil	0.1	
10 10		SAE 20 Motor oil	0.14 to 0.42	
		SAE 30 Motor oil	0.42 to 0.65	
		SAE 40 Motor oil	0.65 to 0.90	
		Glycerine	1.5	
		Pancake syrup	2.5	
10 ¹ – 10 ³ Pastes, gels, and other semisolids (generally non-Newtonian)		Ketchup	≈ 10 ¹	[83]
		Mustard	~ 10	
		Sour cream	≈ 10 ²	
	Peanut butter		[84]	
		Lard	≈ 10 ³	
≈10 ⁸	Viscoelastic polymers	Pitch	2.3 × 10 ⁸	[77]
≈10 ²¹	Certain solids under a viscoelastic description	Mantle (geology)	≈ 10 ¹⁹ to 10 ²⁴	[91]

See also

- Dashpot
- Deborah number
- Dilatant
- Herschel–Bulkley fluid
- High viscosity mixer
- Hyperviscosity syndrome
- Intrinsic viscosity
- Inviscid flow
- <u>Joback method</u> (estimation of liquid viscosity from molecular structure)
- Kaye effect
- Microviscosity
- Morton number
- Oil pressure
- Quasi-solid
- Rheology
- Stokes flow
- Superfluid helium-4
- Viscoplasticity
- Viscosity models for mixtures
- Zahn cup

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Footnotes

- a. The discussion which follows draws from Chapman & Cowling 1970, pp. 232-237
- b. These materials are highly non-Newtonian.

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External links

- Fluid properties (http://webbook.nist.gov/chemistry/fluid/) high accuracy calculation of viscosity for frequently encountered pure liquids and gases
- Gas viscosity calculator as function of temperature (http://www.enggcyclopedia.com/calculators/physical-properties/gas-viscosity/)
- Air viscosity calculator as function of temperature and pressure (http://www.enggcyclopedia.com/calculators/physical-properties/air-v iscosity-calculator/)
- Fluid Characteristics Chart (http://www.engineersedge.com/fluid_flow/fluid_data.htm) a table of viscosities and vapor pressures for

various fluids

- Gas Dynamics Toolbox (http://web.ics.purdue.edu/~alexeenk/GDT/index.html) calculate coefficient of viscosity for mixtures of gases
- Glass Viscosity Measurement (http://glassproperties.com/viscosity/ViscosityMeasurement.htm) viscosity measurement, viscosity units and fixpoints, glass viscosity calculation
- Kinematic Viscosity (https://web.archive.org/web/20100113072736/http://www.diracdelta.co.uk/science/source/k/i/kinematic%20visco sity/source.html) – conversion between kinematic and dynamic viscosity
- Physical Characteristics of Water (http://www.thermexcel.com/english/tables/eau_atm.htm) a table of water viscosity as a function of temperature
- Vogel–Tammann–Fulcher Equation Parameters (http://www.iop.org/EJ/abstract/0953-8984/12/46/305)
- Calculation of temperature-dependent dynamic viscosities for some common components (http://ddbonline.ddbst.de/VogelCalculation/VogelCalculationCGI.exe)
- "Test Procedures for Testing Highway and Nonroad Engines and Omnibus Technical Amendments" (http://www.epa.gov/EPA-AIR/20 05/July/Day-13/a11534d.htm) – United States Environmental Protection Agency
- Artificial viscosity (http://www.astro.uu.se/~bf/course/numhd_course/2_5_2Artificial_viscosity.html)
- Viscosity of Air, Dynamic and Kinematic, Engineers Edge (https://www.engineersedge.com/physics/viscosity_of_air_dynamic_and_kinematic_14483.htm)

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